

## Schottky diodes' relation to technology qualities may affected by external factors

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### ABSTRACT

Additional electric fields (AEF) in Cu-nSi Schottky diodes (SD) of varied diameters that result from the contact surface's constraint with the free surfaces of the contacting materials have a major impact on their electrophysical characteristics. AEF's strong involvement in SD created a functional potential barrier height. AEF's strong involvement in SD created a functional potential barrier height. The current flowing across the contact surface's perimeter and its rest surface determines the forward and initial reverse I-V characteristics of the SD, and this current is well characterised by the thermionic emission theory, as in the idealised homogeneous SD. The effective potential barrier height and contact resistance rose in a forward and primary reverse bias with increasing diameter SD of 6 m to 100 m, while the ideality factor and proportionality coefficient remained almost same. The I-V characteristics of STM images of SD and their contribution to total current of SD demonstrate a rise in peripheral current with increasing reverse voltage. Only peripheral current makes up the second half of the reverse I-V characteristics SD, which is represented as a straight line on a semi-logarithmic scale. The height of the potential barrier, an irrational coefficient, the contact resistance, the size, and the breadth of the contact surface's perimeter are different from those of the first initial section I-V characteristics SD.

**Keywords:** Contact metal – semiconductor, inhomogeneous Schottky barrier, peripheral current Schottky diode, additional electric field, semiconductor converters, limitation of contact surface.

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### INTRODUCTION

Virtual Schottky diodes (SD) are ubiquitous in today's electronics, and their characteristics are the subject of much research. Multifunction capabilities of actual SD showed wide-ranging deviations of parameters and features of the essential data from the core theories and energy models of idealised SD, as a result of extensive study. [1]. Constructive technical approaches to addressing these issues have been successful. SD has led to the creation of a plethora of designs with the express goal of reducing the impact of so-called edge effects, which have traditionally [2]. The breakdown voltage of Al-nSi SDs of varying diameters (20-130 m) and widths (5-50 m) of Al film from the contact edge was studied in [3], where the effect of the width of the metal film on the

surface of the SiO<sub>2</sub> dielectric from the contact edge was examined.

The breakdown voltage of SD was observed to grow from 50V to 90V with an increase in the width of the Al film from 5 μm to 15 μm, and thereafter to remain constant with additional increases in film width. According to the literature [4], the breakdown voltage is tripled from 30V to 130V when the metal electrode is shaped like a cone and makes an angle of around 30° with the silicon surface. Somewhat intriguing are the findings provided in [5], which show that the breakdown voltage rises with the SD when utilising mesa architectures with lateral MOS isolation. An auxiliary electric field (AEF) arises in SD with varying designs because of the restriction of the contact surface with free surfaces of metals and semiconductors. On the Au - nGaAs SD rectangular contact surface, the AEF was measured directly using atomic force microscopy (AFM) and the findings. It is shown that AEF causes an expanded zone (aureole) to develop surrounding the contact, with a potential different from that of the free surface of the nGaAs. Due to the extensive contact area, aureole width may approach 30 μm along a straight metal edge. This is well shown in [6], which demonstrates that the aureole width reduces from 23 μm to 4 μm when the contact-diameter SD is reduced from 100 μm to 5 μm. Relief AFM images of 50 μm diameter Au - nGaAs Schottky diodes, revealing a single gold round contact in exquisite detail. The contact potential difference (CPD) between the edge of a needle cantilever (probe) and a surface Au - nGaAs Schottky diode 50 μm in diameter is shown using AFM pictures. The contact point depth (CPD) on the metal is clearly lower than the CPD on the free surface of nGaAs outside the contact. The contact removal procedure causes the CPD value to rise from its initial low (similar to metal surfaces) to its ultimate high (comparable to the free surface CPD of the semiconductor). As a result, the AEF causes the transitive region (aureole) surrounding the round contacts to have a different CPD width than the CPD of the free semiconductor surface. The AEF is almost ubiquitous in the semiconductor's near-contact area in the narrow SD, where it plays a vital role in the device's electronic operations. The light energy is converted into electrical energy via an Au - nGaAs SD with an AEF converter, where the light current is almost a thousand times higher than the dark current. Light current is around 10 times more than dark current in an analogous SD without AEF. Using an ideality factor near to unity, determined that the reverse current in the SD is negligible at an initial voltage of around 3-4 V.

A more refined plan was devised. TMBS diode, or trench metal oxide semiconductor barrier schottky diode, is a kind of diode in which the whole active emitter field (AEF) is localised in the semiconductor's contact area. The TMBS diode, which is affected by AEF, has higher breakdown voltage compared to standard planar SD, lower leakage current when biased in reverse, and a lower forward voltage. Several investigations [17, 24] indicate a link between the geometrical parameters of the contact surface SD and the potential barrier height. Reducing the diameter of the contact between n- and p-type GaAs in SD form results in a lower potential barrier height Au-nGaAs SD and an increase of the same parameter for p-type GaAs. The whole back side of the wafer had a 300 nm thick layer of tungsten thermally evaporated from a filament at a pressure of  $1 \times 10^{-5}$  Torr. Next, an Ohmic contact with low resistance was made, and the sample was heated to 500 degrees Celsius for three minutes in a nitrogen gas environment. Standard deviation (SD) measurements of static I-V characteristics were taken using a conventional experimental setup at ambient temperature. The usual technique I-V characteristic was used to calculate the SD's

potential barrier height, ideality factor, and specific contact resistance. The peripheral current density  $J_L$  was used to calculate the peripheral parameters  $SD$  and the peripheral contact length  $L$ . The formula was used to calculate the average linear density of peripheral currents  $SD$  over a range of sizes.

ASD in Au-pGaAs. Basic characteristics (the potential barrier height, the ideality factor, the specific capacitance at  $U = 0$ , etc.) in Al-nSi SD [24] were found to be different when  $S > 100$  mm<sup>2</sup>. Mostly unrelated to the SD size. The height of the barrier falls from 0.72 eV to 0.53 eV when the contact area is decreased from 100 mm<sup>2</sup> to 1 mm<sup>2</sup>. As the SD vary in size, the form and size of the contact surface inevitably determines the nature of the AEF's impact. The literature does a terrible job of explaining these aspects of true SD. This study reports the findings of research into the electrophysical characteristics of Cu-nSi Schottky diodes as they relate to the influence of AEF [8].

Here,  $I$  is the current passing through an SD with a contact length of  $L$ ,  $I_e$  is the diameter of a reference SD of 1000 m through which a current of  $I_e$  flows, and  $N$  is the number of SD with a current of  $I$  and a contact length of  $L$ , which adds up to an area equal to that of a reference SD of 1000 m in diameter. Formulas [3] may be used to calculate the areas  $SL$  and breadth  $hL$  of the peripheral contact surface SD for pipes of varying sizes that carry separate peripheral currents  $IL$ :

## **THE EXPERIMENTAL METHODS**

In this study, n-type Si single crystals with a (111) surface orientation and 1 cm resistivity were employed as semiconductor substrates. The Si wafer was degreased by being boiled in trichloroethylene, acetone, and ethanol in rapid succession for 5 minutes before the contacts were made. After being chemically cleaned using the RCA cleaning technique (i.e., a 10-minute boil in  $NH_3 H_2O_2 6H_2O$  followed by a 10-minute boil in  $HCl H_2O_2 6H_2O$ ), the wafer was dipped in diluted HF for 30 seconds, washed in deionized water, and dried with high-purity nitrogen. By evaporating Cu to a thickness of 300 nm in a vacuum environment at a pressure of 1106 Torr, Schottky contacts of varying diameters (6, 10, 20, 60, and 1000 m) were created on the flat surfaces. A digital quartz crystal thickness monitor was used to track the growth of metal layers and the rate of deposition. The rates of deposit ranged from 1-4 Å/s. Aluminum metal with a high degree of purity is immediately available after being cleaned.

As such,  $SO$  denotes the 6-m-diameter contact area surface SD through which the ILO current runs. Using a DualScope TM DS 95-200 / 50, atomic force microscopy (AFM) readings were taken.

## **RESULTS AND DISCUSSION**

Pictures showing SD's current in an STM in both forward and reverse biases. We produced current imaging of a schottky contact in the STM mode of a scanning probe microscope (SPM) system under forward and reverse biases to investigate the method by which current is transported across the patches in MSC contacts operated at various voltages. The forward bias voltage was adjusted from zero to 0.7 V, while the reverse bias voltage was adjusted from zero to -3.0

All patches conduct current under forward bias, and this occurs gradually with increasing applied voltage. The electric fields are amplified or strengthened in the forward bias because they are aligned with the primary electrical fields, although this enhancement has negligible effects on the overall electric field. Nevertheless, the increased electric fields will have a greater impact in the opposite bias. At first, slowly slanting

High-quality I–V characteristics ideal flat SD has the same personality as the empirically observed I–V characteristics, which are depicted by straight lines on a semi-logarithmic scale. The following formula [3] describes them in terms of the thermionic emission hypothesis when  $qU \gg kT$ .

Thermionic emission hypothesis  $f$  is what decides what kind of structures are formed.

This theory states that the maximum potential barrier height SD is at a distance  $m$  from the metal surface, where  $m$  1-2 nm, and that this height is reduced under the influence of the image force, with  $B$  being the height of the ideal potential barrier defined as the difference between the work function of the contacting metal surfaces and the electron affinity of the contacting surface of the semiconductor. Unlike the I–V characteristics of an ideal flat SD, the I–V characteristics of Cu–nSi DS with diameters of 6, 10, 20, 60, and 100  $m$  exhibit various distinctive traits, as shown by forward and reverse current flow investigations. Favoring the future. The semi-logarithmic forward I–V characteristics of Cu-nSi SD of varying diameters that were all manufactured using the same technology. A curve's diameter is a defining parameter. Indeed, it's plain to observe

Area of contact ( $S$ ), temperature ( $T$ ), Boltzmann constant ( $k$ ), and electron charge ( $q$ ) are all variables in this equation.  $U$  is the applied voltage and  $A$  is the effective potential barrier height,  $nf$  is the ideality factor, and  $f$  is the proportionality coefficient for varying the barrier height with voltage.

The forward current–voltage characteristics of Cu–nSi DS of varying diameters, whereas The dependency of current on contact diameters SD at varying voltages (b).

In this context, the values of  $A$  and  $T$  are  $120A \cdot m^{-2} K^{-2}$  and  $300K$ , respectively. There is a rise in the effective potential barrier height and the contact resistance from an SD diameter of 6  $m$  to 100  $m$ , although the ideality factor and proportionality coefficient are mostly unaffected. These correlations originate from the fact that the amount of AEF exerted on a contact varies with its size. The relationship between the current SD and the diameter of the contacts at various voltages, which may be used to calculate the impact of the peripheral current SD. From the pictures, we may deduce that straight lines can be used to depict these curves, and that the slope of these lines is less than 2. These findings validate and quantify the results of the computation of peripheral parameters SD, demonstrating the importance of the observed lines I-V features of SD in characterising the current total area of the contact surface and the peripheral current contribution to the total current SD.

The formulas used to determine the average linear density  $J_{LF}(0)$  of the current flowing through the periphery SD at  $U = 0$ ; the area ( $SL$ ) and width ( $hL$ ) of the peripheral contact surface (where,

$hL = SL / L$ , when  $L \gg d$ ); the potential barrier height ( $L$ ); and the contribution ( $GL$ ) of the peripheral current to the total current ( $DS$ ) (i.e., the ratio of the peripheral current ( $IOL$ ) to the total current). We can observe that the  $JLF(0)$  shares values on the order of  $10^{11} \text{ A / m}$  with  $DS$ s with varying diameters. This indicates that for  $SD$  of varying diameters, the possible barrier height close to the contact's edge is essentially constant. At the contact  $SD$ 's edges, the potential barrier is roughly  $40 \text{ meV}$  lower than it is in the centre. The forward bias currents in the  $\text{Cu-nSi}$   $DS$  with the experimental data provided above. As in the idealised  $DS$ , the effective barrier height  $F$  is used to define the boundary between the contact area and the free surfaces of the contacting materials. With increasing distance from the centre, the barrier height  $BL$  decreases to  $F$  throughout the whole contact surface of the  $SL$ , which has a width of  $hL$  and is sized according to  $SD$ . In addition, when the contact widths shrank, a larger fraction of the total current  $SD$  was contributed by the electrodes' periphery. Bias in the other direction. We see the typical reverse  $-V$  characteristics of  $\text{Cu-nSi}$   $SD$ s of varying diameters. Two distinct ranges of voltage are shown for the  $SD$ : the first, from zero to approximately one volt, and the second, from about one volt up to the breakdown voltage. For  $SD$  of varying diameters, the first portion of the  $I-V$  characteristics shows a gradual rise in current as a function of voltage  $U$ .

The electrophysical parameters of the inverse  $I-V$  characteristics of  $SD$ s of varying diameters were determined using formulae (9) and (10).

Using forward  $I-V$  characteristics  $SD$ , we can establish that the diameters are about equivalent to the height of the barrier. As the  $SD$  grew in size, the dimensionless coefficients ( $nr$ ) went up, but the proportionality coefficient ( $r$ ) went down. Similar to the results shown in forward bias, the obtained in reverse bias generated various degrees of effect on the AEF depending on the diameter of the contact.

The study's findings, Straight lines illustrate the dependency between the current  $IR$  and the contact diameter  $SD$  throughout a range of voltages. At voltages up to 3, the slope of this straight line is close to minus 2. The slope is lowered to 1 as the voltage is increased. This indicates that only currents running around the periphery of the contact surface contribute to the total  $SD$  current. Contribution of the  $GL$  peripheral current to the  $SD$  total current over a range of voltages and diameters. At  $U > 8V$ , the total current  $SD$  for contacts of varying diameters consists entirely of current flowing around the contact's perimeter, a phenomenon that increases with voltage. We see the inverse  $I-V$  characteristics  $SD$  plotted against diameter on a semi-logarithmic scale. Straight lines, like the forward  $I-V$  characteristics  $SD$ , depict the reliance above  $6V$  in the image. The formula [19] for the current along the  $SD$ 's perimeter, which is determined by a thermionic emission process, is as follows:

As a result, it became evident that the current flow in the reverse-bias  $\text{Cu-nSi}$   $SD$  with a limiting contact surface is quite different from the current flow in the idealised  $SD$ . Adding the currents flowing through the outside surface of a certain width ( $IL$ ) and the remaining inner section of the contact surface yields the reverse current ( $IR$ )  $SD$ . When comparing the electrophysical properties of the contact surface  $SD$ 's interior and outside, the differences are striking. Similarly, the fundamental distinction between the interior and peripheral regions of the contact surface  $SD$  in

the barrier height dependency on the applied voltage is of considerable importance.

## CONCLUSION

The electrophysical characteristics of Cu-nSi SD vary greatly depending on the diameter, and this variation is mostly attributable to AEF that develops as a result of the contact surface's inability to fully engage with the free surfaces of the contacting materials. During SD, the presence of AEF generated a powerful potential barrier. As in the idealised homogeneous case, forward and initial reverse I-V characteristics SD are determined by the current flowing through the periphery of the contact surface as its rest surface.

SD. Effective potential barrier contact resistance increased in forward and primary reverse bias as SD grew in size from 6 m to 100 m, but ideality was maintained throughout.

Specifically, we have  $L = SL * hL * U$ , where  $SL$  is the area of the peripheral contact surface,  $hL$  is the width of the contact,  $nL$  is the dimensionless coefficient,  $L$  is the proportionality coefficient, and  $U$  is the applied voltage. As a result, the saturation current of IOLs of varying diameters  $D$  was calculated by extrapolating straight lines to the ordinate axis. Dimensionless coefficient  $nL$  and proportionality coefficient  $L$  for SD with varying diameters were computed, as well as the barrier height for peripheral SD, using equations (2) and (3). The I-V characteristics, which made use of ILO and  $SL$ , determined the height of the barrier. According to a formula developed to mirror the forward I-V characteristics DS definition, the dimensionless coefficient and the proportionality coefficient were calculated.

both the factor and the proportionality coefficient have kept their original values. The STM images of SD and their I-V characteristics demonstrate that, as reverse voltage is increased, a larger fraction of the total current of SD originates from the device's periphery. On the other hand, the SD part of the reverse I-V characteristics is a straight line on a semi-logarithmic scale since it only contains the peripheral current. Differences exist between the I-V characteristics SD of the first initial segment and the characteristics of the rest of the contact surface in terms of potential barrier height, a dimensionless coefficient, contact resistance, area, and perimeter width. The varying degrees of influence AEF arising in the near-contact region of semiconductor explain the dependence of electrophysical parameters and characteristics of SD on the diameters of contacts.

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